

Air Quality Permitting Technical Memorandum

November 25, 2002

Tier II Operating Permit and Permit To Construct No. 005-00004 Ash Grove Cement Company, Inkom

T2-010313

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FINAL PERMIT

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ACRONYMS, UNITS, AND CHEMICAL NOMENCLATURE

Aerometric Information Retrieval System AIRS

AIRS Facility System AFS Air Quality Control Region AQCR British thermal unit(s) Btu

Clean Air Act CAA

Code of Federal Regulations CFR

carbon monoxide CO

Department of Environmental Quality DEQ

dry standard cubic foot or feet dscf

emission factor EF

Environmental Protection Agency EPA

fugitive dust FD fugitive emissions FE foot or feet ft

gallons per minute gpm

grain(s) gr

grains per dry standard cubic foot gr/dscf

Hazardous Air Pollutants **HAPs**

hour(s) hr

A numbering designation for all administrative rules in Idaho promulgated under the **IDAPA**

Idaho Administrative Procedures Act

in.

ISCST3 Industrial Source Complex Short Term 3

kilogram kg kj kilojoules kilometers km kilowatts kW pound per hour lb/hr meter(s) m

 m^3 cubic meter(s)

mg/m³ milligrams per cubic meter

micrometers μm

Maximum Achievable Control Technology MACT

minute(s) min

million British thermal units per hour MMBtu/hr National Ambient Air Quality Standards NAAQS

NESHAP National Emission Standards for Hazardous Air Pollutants

nitrogen dioxide NO₂ nitrogen oxides NO_X

New Source Performance Standards **NSPS**

ozone O₃ percent % Pb lead

particulate matter PM

particulate matter with an aerodynamic diameter less than or equal to a nominal 10 PM₁₀

micrometers

PSD Prevention of Significant Deterioration

PTC permit to construct ppm parts per million second(s)

Source Classification Code SCC

| scf | standard cubic feet |
|-----------------|------------------------------|
| SIP | State Implementation Plan |
| SO ₂ | sulfur dioxide |
| TAP | Toxic Air Pollutant |
| T/yr | tons per year |
| TSP | total suspended particulates |
| U.S. | United States |
| VOC | volatile organic compound |
| Wt% | percent by weight |
| vr | vear(s) |

PURPOSE

The purpose for this memorandum is to satisfy the requirements of IDAPA 58.01.01 Sections 200 - 223, Rules for the Control of Air Pollution in Idaho for permits to construct and Sections 400 - 470 for Tier II operating permits.

PROJECT DESCRIPTION

This project is for the modification of Tier II Operating Permit No. 004-00005 for Ash Grove Cement Company (Ash Grove) located at Inkom, Idaho. Ash Grove is requesting an increase in allowable iron ore usage from its current rate of 4,841 T/yr to 7,000 T/yr. Due to Ash Grove's previous error in the iron ore usage calculation, an erroneously low annual iron ore usage rate was submitted and permitted. Ash Grove also requested increased hourly CO emission limits.

The project also involves incorporating Ash Grove's two PTCs, issued January 29, 1999, and May 17, 1999, into the Tier II Operating Permit. Ash Grove did not request that this be done. DEQ decided to include the PTCs in an attempt to avoid confusion over the emission limits. The January 29, 1999 PTC includes an emission limits table that supercedes the emission limits table in the 1997 Tier II. Therefore, this project will include all the current emission limits and operating/monitoring requirements from the existing permits in the Tier II, except for initial compliance testing requirements from the PTCs. The Tier II expiration date will remain the same (December 8, 2002) because this project is not a renewal.

This project does not include Ash Grove's request to replace the #1 coal mill and modify the #1 and #2 cement finish mill dust collector (T2-990005a). That request was received by DEQ on June 24, 1999, and was determined incomplete until adequate modeling is received. This project also does not include Ash Grove's request to modify the Tier II to reflect the rerouting of silica and gypsum and the installation of a quarry stacking belt. According to DEQ's letter dated August 14, 2000, that permitting action is also suspended until the modeling analysis is received.

SUMMARY OF EVENTS

| **** | |
|---------------------------------------|--|
| August 15, 2001 | DEQ received an application from Ash Grove for a modification to Tier II Operating Permit No. 004-00005, issued December 8, 1997. The project was activated from the backlog of permitting actions on March 22, 2002. |
| April 2, 2002 | The application was declared complete. |
| June 24, 2002 – July 25, 2002 | A public comment period on the draft permit was held. No comments were received during that period. |
| May 24, 2002 | DEQ received from Ash Grove a modeling analysis and request to increase the hourly CO emission limits for the kilns. |
| July 19, 2002 | The modeling analysis with the increased CO emission limits was determined to demonstrate compliance with the NAAQS. Rather than issue separate permits for each modification, DEQ has decided to include the increased CO emission limits in the draft permit and send the permit out for public comment again. |
| September 4, 2002- October 3, 2002 | A second public comment period on draft permit was held. Comments were received from Ash Grove and are provided in Appendix C. |

A second public comment period on draft permit was held.

Comments were received from Ash Grove and are provided in Appendix C.

The comments request that the permit include the June 10, 2002 consent order requirements to avoid conflict between the consent order language and the Tier II operating permit. The comments also request that the permit expiration date be extended to allow for issuance of the new Tier II required by the consent order. The consent order requires Ash Grove to submit a complete application to modify the Tier II operating permit within 180 days of the effective date of the consent order. One hundred eighty days from June 10, 2002 is December 8, 2002, which is the same day the permit expires. As noted in IDAPA 58.01.01.404.04, the

expiration of a Tier II permit will not affect the operation of a stationary source or a facility during the administrative procedure period associated with the permit renewal process. Therefore, the expiration date does not need to be extended.

A Tier I Operating Permit for Ash Grove Cement's Inkom facility is scheduled to be issued before January 2003. The Tier I permit will include all requirements in the Tier II operating permit.

FACILITY DESCRIPTION

General Process Description

The *Iron Ore Receiving, Crushing, and Storage* emissions unit is the subject of this modification. The manufacture of Portland cement requires a very specific chemical mixture. Limestone, silica/shale, iron ores, and clay materials are proportioned to achieve the proper chemical mixture. Ash Grove discovered that the amount of iron ore permitted is not adequate to maintain the chemical mixture required so they asked for an increase.

Facility Classification

The facility is a designated facility as defined in IDAPA 58.01.01.006.27 (Portland Cement Plant). The AIRS Facility Subsystem classification is A because potential emissions of PM_{10} , SO_2 , NO_x and CO are greater than 100 tons per year. The facility is subject to PSD permitting requirements for a major modification because the facility's PTE is greater than 100 T/yr. This facility is a portland cement manufacturer, SIC code 3241.

Area Classification

Ash Grove Cement Company, Bannock county Idaho, is located in AQCR 61. The area is classified as attainment or unclassifiable for all federal and state criteria air pollutants (i.e., PM₁₀, SO_x, O₃, NO₂, CO, and Pb). There are no class I areas within 10 km of the facility.

TECHNICAL ANALYSIS

1. <u>Emissions Estimates</u>

The emissions limits for the iron ore process in the 1997 Tier II permit were set much higher than the calculated potential emission rate (see Table 1.1). The same spreadsheet that was used in the 1997 tech memo was used to calculate the new allowable emissions. The hours per year of operation were changed from 24 to 36 and the annual throughput was changed from 4,841 tons to 7,000 tons. All other inputs to the spreadsheet remained the same. The emission limits in the Tier II permit will be decreased and set at 100% of expected potential emissions. Emissions calculations for iron ore are provided in Appendix A.

| | PM. PM. | | | | | | | | |
|------------------------------|---------|--------|-------|--------|--|--|--|--|--|
| | lb/hr | ton/yr | lb/hr | ton/yr | | | | | |
| Old Ilmits | 16,38 | 0.16 | 7.14 | 0.07 | | | | | |
| 1999 actual emissions | 1.72 | 0.03 | 0.82 | 0.01 | | | | | |
| 2000 actual emissions | 1.97 | 0.04 | 0.95 | 0.02 | | | | | |
| Average of 1999-2000 | 1.85 | 0.035 | 0.89 | 0.015 | | | | | |
| New limits (potential) | 2.26 | 0.04 | 1.08 | 0.02 | | | | | |
| Change (actual to notential) | 0.41 | 0.005 | ∩ 1Q | 0.005 | | | | | |

Table 1.1 OLD AND NEW IRON ORE PROCESS EMISSION LIMITS

In a letter received May 24, 2002, Ash Grove requested that the 1-hour CO emission limits for the kilns be increased. The old and new CO emission limits are listed in Table 1.2

Table 1.2 OLD AND NEW KILN CO EMISSION LIMITS

| ALCOHOLD IN THE | aros es generale Kiln | No. 1 | Se Kilin Na | 2 |
|--|------------------------------|----------|--------------------------|-----------|
| THE PROPERTY OF THE SAME OF TH | ::: Ib/hrfa:::: | ton/yr 🛸 | to ear lib/his seasons a | ≁∉ ton/yr |
| Old limits & excels | 234.4 | 937.7 | 275.8 | 1103.2 |
| New limits are reacted. | 550 | 937.7 | 650 | 1103.2 |
| Increase with a comment | 315.6 | 0 | 374.2 | 0 |

New limit is based on a 1-hour average.

2. Modeling

No modeling is required for the iron ore modification because the allowable emission rates in the old Tier II permit, issued December 8, 1997, were greater than the new potential emissions. The allowable emissions in the Tier II decreased significantly and are now set to accurately reflect potential emissions.

The modeling analysis for the CO emission limit increase was reviewed by DEQ. The results of the review are presented in Appendix B.

3. Regulatory Review

- Iron Ore Receiving, Crushing, and Storage
- Emissions Limit (Permit Condition 2.1.1, page 5)

The PM₁₀ SIP permit contains pound per hour and ton per year fugitive emission limits for the *Iron Ore Receiving, Crushing, and Storage* process

Compliance Demonstration

Compliance with the pound per hour and ton per year emission limits is demonstrated by not exceeding the iron ore processing rates of 200 T/hr and 7,000 T/yr. Compliance with the emission limits is shown through engineering calculations using AP-42 emission factors and control efficiencies for partial enclosure and moisture in the ore. The engineering calculations are provided in the appendix. The spreadsheet containing the calculations was developed in 1997 as explained in the emissions estimates section.

4. NSPS Applicability

The Standards of Performance for Portland Cement Plants (40 CFR 60 Subpart F) do apply to the conveyor transfer points which are part of the iron ore receiving, crushing, and storage emissions unit. As Ash Grove acknowledges in the application, the opacity limit from the transfer points is 10%.

NESHAPS Applicability

According to Ash Grove's Tier I permit application, the Inkom facility is an area source of HAPs. Therefore, no requirements of the NESHAP (40 CFR 63 Subpart LLL) are applicable to the iron ore receiving, crushing, and storage emissions unit. The only affected units at an area source are the kilns.

6. AIRS

AIRS/AFS^a FACILITY-WIDE CLASSIFICATION^b DATA ENTRY FORM

| AIR PROGRAM | | | | | | 2772 | AREA CLASSIFICATION A – Attainment |
|-------------------------------|------|------------------|------------------------|---------------------|--------------------------------|------------|---|
| POLLUTANT | SIP® | PSD ⁴ | NSPS * (Part 60) | NESHAP (Part 61) | MACT ⁹ (Part 63) | TITLE V | U – Unclassifiable N – Nonattainment |
| SO ₂ h | Α | Α | | | | Α | A |
| No _x ^I | Α | Α | | | | Α | А |
| co, | Α | A | | | | Α | A |
| PM ₁₀ * | Α | A | | | | Α | Α |
| PT (Particulate) ^I | Α | Α | Α | | | Α | |
| voc " | В | В | | | | Α | |
| THAP (Total HAPs) " | | | | | | | |
| | | | APF | LICABLE SUB | PART | | |
| | | | F | | LLL | | |

Aerometric Information Retrieval System (AIRS) Facility Subsystem (AFS)

AIRS/AFS Classification Codes:

- A = Actual or potential emissions of a pollutant are above the applicable major source threshold. For NESHAP only, class "A" is applied to each pollutant which is below the 10 ton-per-year (T/yr) threshold, but which contributes to a plant total in excess of 25 T/yr of all NESHAP pollutants.
- SM = Potential emissions fall below applicable major source thresholds if and only if the source complies with federally enforceable regulations or limitations.
- B = Actual and potential emissions below all applicable major source thresholds.
- C = Class is unknown.
- ND = Major source thresholds are not defined (e.g., radionuclides).
- ^c State Implementation Plan
- Prevention of Significant Deterioration
- * New Source Performance Standards
- National Emission Standards for Hazardous Air Poliutants
- ⁹ Maximum Achievable Control Technology
- ^h Sulfur Dioxide
- Nitrogen Oxides
- Carbon Monoxide
- Particulate matter with an aerodynamic diameter less than or equal to a nominal 10 micrometers
- Particulate Matter
- M Volatile Organic Compounds
- ⁿ Hazardous Air Pollutants

FEES

Fees apply to this facility in accordance with IDAPA 58.01.01.470. The facility is subject to permit application fees for this revised Tier II Operating Permit of \$500.

RECOMMENDATIONS

Based on the review of the application materials, and all applicable state and federal regulations, staff recommends that DEQ issue a modified Tier II operating permit and PTC to Ash Grove Cement Company. Staff members have notified the facility in writing of the required Tier II application fee of five hundred dollars (\$500.00). The permit will be issued upon receipt of the fee.

ZK/sm

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cc:

Laurie Kral, EPA Region 10

Tiffany Floyd, Pocatello Regional Office

APPENDIX A

Emission Estimates

| 71077 | | | THROUGHPUT | | | | | | EMISSION FACTORS | | | | | | EMISSIONS | | | | | |
|---|---------------------|--|--|------------------|--|-----------|----------|--|------------------|-------------|---------|----------------|--------------|--------------|--------------|----------|---------------|---------------|----------------|---------|
| COURCE | DESCRIPTION | | ubc. | DAYS | HRS | 71 HOUGH | MAX. | AVG | | TSP | PM10 | T | PM10 | | ONTRO | | TS | | PM | 10. 1 |
| | NAME FROM | NAME TO | /DAY | | | MATERIAL | TON/H | | TON/YR | LB/TON | L8/TON | PEE | | | | | LB/HR | | LB/HR | |
| | | | / DAT | /11/ | /// | mm: Chial | 10/1/11 | IVN/A | 3017/IN | LDITOR | LOTION | PAGE. | 11777 | 11(0)0). | | DOILD. | 2071111 | 17.111 | 3400000 | |
| | 3, BLASTING AND DOZ | The state of the s | 24 | | 300 | LIMESTONE | | | 435,708 | 0.0003 | 0.0001 | | 36% | 0% | 0% | 0% | | 0.06 | ├ | 0.02 |
| | DRILLING | | | <u> </u> | | | | | | 0.0003 | 0,0001 | | 3076 | | | | | 0,00 | | |
| <u>F 2</u> | BLASTING | I | 24 | 0 | | LIMESTONE | | | 435,708 | | | l b | 40.00 | 0% | 0% | 096 | | | } | 0.00 |
| F 3 | DOZING | D9L | <u> </u> | ! | | LIMESTONE | | | 435,708 | 0.0029 | 0.0014 | <u> 2 </u> | 48% | | | | ├── ┤ | 0.00 | ļ | |
| | | DION | ļ | | 1,955 | LIMESTONE | · | | 435,708 | 0.0029 | 0.0014 | C. | 48% | ļi | <u> </u> | <u> </u> | ļļ | 0.00 | <u> </u> | 0.00 |
| | | | ļ | | | | <u> </u> | | | | | <u> </u> | <u> </u> | | | Totals: | Įi | 0.06 | ļ | 0.02 |
| | HE RECEIVING, CRUSH | | | <u> </u> | | | | | | | | <u> </u> | L | | | | <u> </u> | | <u> </u> | |
| F 4 | LOADER | FEEDER | 8 | | | LIMESTONE | 200 | 159 | 435,708 | 0.0002 | 0.0001 | | 48% | 0% | 0% | 80% | 0.01 | 0.01 | 0.00 | 0.00 |
| F 5 | FEEDER | JAW CRUSHER | 8 | | | LIMESTONE | 200 | 159 | 435,708 | 0.0007 | 0.0003 | c | 48% | 50% | 0% | 90% | 0.01 | 0.01 | 0.00 | 0.00 |
| f 6 | JAW CRUSHER | #1 INCLINE BELT | 8 | 343 | | LIMESTONE | 200 | 159 | 435,708 | 0.0029 | 0.0014 | | 48% | 50% | 0% | 90% | 0.02 | 0.03 | 0.01 | 0.02 |
| F 7 | #1 INCLINE BELT | #2 INCLINE BELT | 8 | 343 | 2,741 | LIMESTONE | 200 | 199 | 544,635 | 0.0029 | 0.0014 | j c | . 48% | 50% | 0% | 60% | 0.12 | 0.16 | 0.06 | 0.08 |
| F 14 | #2 INCLINE BELT | SCREEN #1 | 8 | 361 | 2,891 | LIMESTONE | 200 | 188 | 544,635 | 0.0029 | 0.0014 | ¢ | 48% | 20% | 0% | 90% | 0.04 | 0.06 | 0.02 | 0.03 |
| F 15 | SCREEN #1 | CROSS CTRY. BELT | 8 | 361 | 2,891 | LIMESTONE | 200 | 151 | 435,708 | 0.0029 | 0.0014 | ¢ | 48% | 20% | 0% | 90% | 0.04 | 0.05 | 0.02 | 0.02 |
| F 16 | SCREEN #1 | HAMMER MILL | 8 | 361 | 2,891 | LIMESTONE | 200 | 38 | 108,927 | 0.0007 | 0.0003 | T c | 48% | 20% | 0% | 90% | 0.00 | 0.00 | 0.00 | 0.00 |
| F 17 | HAMMER MILL | #1 INCLINE BELT | 8 | 361 | | LIMESTONE | 200 | 38 | 108,927 | 0.0029 | 0.0014 | ¢ | 48% | 50% | 0% | | 0.01 | 0.01 | 0.00 | 0.00 |
| F 18 | CROSS CTRY, BELT | BELT B | 8 | 361 | | LIMESTONE | 200 | 151 | 435,708 | 0.0029 | 0.0014 | | 48% | 20% | 0% | | | 0.51 | 0.17 | 0.24 |
| F 19 | BELT B | BELT C | 8 | 361 | | LIMESTONE | 200 | 151 | 435,708 | 0.0029 | 0,0014 | | 48% | 20% | 0% | | 0.35 | 0.51 | 0.17 | 0.24 |
| F 20 | BELT C | SILOS (3) | 8 | 361 | | LIMESTONE | 200 | 151 | 435,708 | 0.0029 | 0.0014 | | 48% | 20% | 0% | | | 0.05 | 0.02 | 0.02 |
| | LE CRUSHED ROCK: | | † | 1 | | | 1 | 1 | | | | 1 - | 1 | X | | T~ | | | 1 | |
| | CROSS CTRY, BELT | CHUTE | 8 | 25 | 200 | LIMESTONE | 200 | 200 | 40,000 | 0.0029 | 0.0014 | c | 48% | 20% | 0% | 0% | 0.47 | 0.05 | 0.22 | 0.02 |
| F 25 | CHUTE | GROUND | 1 8 | 25 | | LIMESTONE | 200 | 200 | 40,000 | 0.0029 | 0.0014 | | 48% | | 0% | | 0.47 | 0.05 | 0.22 | 0.02 |
| ' ** | 10110 : L | W. | | 1-25 | | LIMESTOTE | | **** | 47,000 | U.VVE3 | 9.0014 | ┿┈ | | 2070 | 1 720 | Totals: | | 1.49 | | 0.72 |
| IDOM | OOF DECEIVING | CRUSHING AND | ÉTA | DACE | 11000 | Astroll | <u> </u> | | | | | + | | | | 1 | 7.77 | 11 | 7777 | |
| | | <u></u> | | | | | <u> </u> | | | <u> </u> | | <u> </u> | <u> </u> | | <u> </u> | <u> </u> | | | <u> </u> | |
| F 4 | LOADER | FEEDER | 2 | 16 | | IRON ORE | 200 | 148 | 5,324 | 0.0002 | 0.0001 | | 48% | 0% | 0% | | 0.01 | 0.00 | 0.00 | |
| F 5 | FEEDER | JAW CRUSHER | 2 | 18 | | IRON ORE | 200 | 148 | 5,324 | 0.0007 | 0.0003 | | 48% | | 0% | 90% | | 0.00 | 0.00 | 0.00 |
| F 6 | JAW CRUSHER | #1 INCLINE BELT | 2 | 18 | 36 | IRON ORE | 200 | 148 | 5,324 | 0.0029 | 0.0014 | ¢ | 48% | 50% | 0% | 90% | 0.02 | 0.00 | 0.01 | 0.00 |
| F 7 | #1 INCLINE BELT | #2 INCLINE BELT | 2 | 18 | 36 | IRON ORE | 200 | 148 | 5,324 | 0.0029 | 0.0014 | ¢ | 48% | 50% | 0% | 60% | 0.09 | 0,00 | 0.04 | 0.00 |
| F 8 | #2 INCLINE BELT | #3 INCLINE BELT | 2 | 18 | 36 | IRON ORE | 200 | 148 | 5,324 | 0.0029 | 0.0014 | C | 48% | 20% | 0% | 90% | 0,03 | 0.00 | 0.02 | 0.00 |
| F 9 | #3 INCLINE BELT | SCREEN #2 | 2 | 18 | 36 | IRON ORE | 200 | 148 | 5,324 | 0.0313 | 0.0150 | C | 48% | 20% | 0% | | 0.37 | 0.01 | 0.18 | 0.00 |
| F 10 | SCREEN #2 | CROSS CTRY, BELT | 2 | 18 | 36 | IRON ORE | 200 | 148 | 5,324 | 0.0029 | 0.0014 | 1 6 | 48% | 20% | 0% | | | 0.00 | 0.02 | 0.00 |
| F 11 | SCREEN #2 | CONE CRUSHER | 2 | Ó | - | IRON ORE | - | n/a | , | 0.0029 | 0.0014 | c | 48% | 20% | 090 | | | * | T | |
| F 12 | CONE CRUSHER | #4 INCLINE BELT | 2 | 0 | | IRON ORE | T : | n/a | | 0.0029 | 0.0014 | | 48% | 20% | 0% | | | 1 | ļ . | · · |
| F 13 | #4 INCLINE BELT | #2 INCLINE BELT | 2 | Ö | | RON ORE | † | n/a | | 0.0029 | 0.0014 | | 48% | | 0% | | | ! | | - |
| F 14 | #2 INCLINE BELT | SCREEN #1 | 2 | 18 | 36 | IRON ORE | 200 | 148 | 5.324 | 0.0313 | 0.0150 | | 489 | | 0% | | | 0.01 | 0.18 | 0.00 |
| F 15 | SCREEN #1 | CROSS CTRY, BELT | 2 | 18 | 36 | IRON ORE | 200 | 148 | 5,324 | 0.0029 | 0.0014 | C | 489 | | 0% | | 0.03 | 0.00 | 0.02 | 0.00 |
| F 16 | SCREEN #1 | HAMMER MILL | 2 | 18 | | IRON ORE | 200 | 148 | 5,324 | 0.0007 | 0.0003 | | 489 | | 090 | | | 0.00 | | |
| F 17 | HAMMER MILL | #1 INCLINE BELT | 2 | 18 | | IRON ORE | 200 | 148 | 5,324 | 0.0029 | 0.0014 | | 489 | 50% | 0% | | | | | |
| F 18 | CROSS CTRY, BELT | BELT B | 2 | 18 | | IRON ORE | 200 | 148 | 5.324 | 0.0029 | 0.0014 | | 489 | | | | | | | |
| F 19 | BELT B | BELT C | 2 | 18 | | IRON ORE | 200 | 148 | 5,324 | 0.0029 | 0.0014 | | 489 | | | 098 | | | | |
| F 20 | BELT C | SiLO\$ (3) | 7 2 | | | RON ORE | 200 | 148 | 5,324 | 0.0029 | 0.0014 | | 489 | | 090 | 90% | | | | |
| | | | 1 | † - - | | | 1 | | T | 1 | 1 | ┪ | 1 | 1 | 1 | Totals | | | | |
| SILICA | ECEIVING, CRUSHING | AND STORAGE | 1 | 1 | ''' | 1 | 1 | 1 | i | T | 1 | _ | + | · | 1 | 1 | 1 | | 1 | |
| F 4 | LOADER | FEEDER | 1 4 | 55 | 210 | SILICA | 200 | 200 | 43,571 | 0.0002 | 0.0001 | - c | 489 | 0% | 0% | 80% | 0.01 | 0.00 | 0.00 | 0.00 |
| F 5 | FEEDER | JAW CRUSHER | 1 7 | | | SILICA | 200 | 200 | 43,571 | 0.0007 | 0.0003 | | 489 | | | | | | | |
| | JAW CRUSHER | #1 INCLINE BELT | 7 | | | SILICA | 200 | | 43,571 | 0.0029 | | | | | | | | | | |
| F 6 | | | | | | | | 200 | | | 0.0014 | | 489 | | | | | | | |
| F 7 | #1 INCLINE BELT | #2 INCLINE BELT | <u> </u> | | | SILICA | 200 | 200 | 43,571 | 0.0029 | 0.0014 | | 489 | | | | | | | |
| F B | #2 INCLINE BELT | #3 INCLINE BELT | 4 | | | SILICA | 200 | 200 | 43,571 | 0.0029 | 0.0014 | | 489 | | | | | | | |
| f 9 | #3 INCLINE BELT | SCREEN #2 | 4 | | | SILICA | 200 | 200 | 43,571 | 0.0313 | 0.0150 | | 489 | | | | | | | |
| F 10 | SCREEN #2 | CROSS CTRY, BELT | 4 | | | SILICA | 200 | 200 | 43,571 | 0.0029 | 0.0014 | | 489 | | | | | | | |
| F 11 | SCREEN #2 | CONE CRUSHER | 4 | | | SILICA | 200 | 200 | 43,571 | 0.0007 | 0.0003 | | 489 | | | | | | | |
| F 12 | CONE CRUSHER | #4 INCLINE BELT | 4 | | | SILICA | 200 | ,500 | 43,571 | 0.0029 | 0.0014 | | 489 | | | | | | | |
| F 13 | #4 INCLINE BELT | #2 INCLINE BELT | 4 | 55 | | SILICA | 200 | 200 | 43,571 | 0.0029 | 0.0014 | c | 489 | 20% | | | | 0.05 | 0.22 | |
| F 18 | CROSS CTRY. BELT | BELT B | 4 | 55 | 218 | SILICA | 200 | 200 | 43,571 | 0.0029 | 0.0014 | C | 489 | 20% | | | | 0.05 | 0.22 | 0.02 |
| F 19 | BELT B | BELT C | 4 | | | SILICA | 200 | 200 | 43,571 | 0.0029 | 0.0014 | | 489 | | | | | 0.05 | 0.22 | 0.02 |
| F 20 | BELT C | SILOS (3) | 4 | | | SILICA | 200 | | 43,571 | 0.0029 | | | 489 | | | | | | | |
| F 24 | CROSS CTRY, BELT | CHUTE | 8 | | | SILICA | 200 | | 43,571 | | | | 489 | | | | | | | |
| : L0t.7 | | | | | | | | | | | | | | 77.77 | | | | | | |

| 7 | | | ··· <u>·</u> | | | THROUGHP | ŧIT | | | · | F) | MISSIO | N FACTO |)RS | | | | EMISS | SIONS | |
|------------|---------------------|------------------|--|--|--------------|--------------|---------------|--------------|--------------|--------------|--|----------------|--------------|------------|-------------|--------------|--|--------------|-------------|--------------|
| COURCE | DESCRIPTION | | HPS | DAYS | HRS | 111111111111 | MAX. | AVG. | | TSP | PM10 | 1 | PM10 | | ONTROL | | TS | | PM | 10 |
| | NAME FROM | NAME TO | /DAY | | | MATERIAL | TON/H | | TON/YR | LB/TON | | RFF | | | | | LB/HR | T/YR | LB/HR | |
| | , BLASTING AND DOZ | | 1001 | 7377 | / 1+1 | HOTT LINETE | 101011 | 1911/11 | 10,77,111 | 227 7031 | 4011011 | 1 112 | 111101 | 77.07.41.1 | 2012 11 | D W 1 C D 1 | - W-7 - 1 1 1 | | | |
| PAILE TIME | DRILLING | 174 | 24 | 0 | 220 | LIMESTONE | | | 435,708 | 0,0003 | 0.0001 | • | 36% | 0% | 0% | 0% | | 0.06 | ļ | 0.02 |
| <u> </u> | | ·} | | | 320 | | | | | 0.0003 | U.U.VA | | -222 | | | | | 0.00 | | <u> </u> |
| <u> </u> | BLASTING | 1 | 24 | 0 | | LIMESTONE | <u> </u> | | 435,708 | - 4 4 4 4 4 | ~~~~~ | b | | <u> </u> | 0% | 0% | | ~ ~ ~ ~ | | 0.00 |
| F 3 | DOZING | D9L | <u></u> | jj | | LIMESTONE | ļj | | 435,708 | 0,0029 | 0.0014 | C | 48% | | | | ļj | 0.00 | ļ | |
| | | DION | | | 1,955 | LIMESTONE | ļ | | 435,708 | 0.0029 | 0.0014 | C | 48% | | | | | 0.00 | ļ | 0.00 |
| | | | <u> </u> | <u></u> | | | | | | | | | | | | Totals: | - | 0,06 | • | 0.02 |
| | NE RECEIVING, CRUSH | | L | | · | | | | | | | 1 | | | | | | | | |
| F 4 | LOADER | FEEDER | | 343 | | LIMESTONE | 200 | 159 | 435,708 | 0.0002 | 0.0001 | C | 48% | 0% | 0% | 80% | 0.01 | 0.01 | 0.00 | 0.00 |
| F 5 | FEEDER | JAW CRUSHER | - 8 | | | LIMESTONE | 200 | 159 | 435,708 | 0.0007 | 0.0003 | ¢ | 48% | 50% | 0% | 90% | 0.01 | 0.01 | 0.00 | |
| F 6 | JAW CRUSHER | #1 INCLINE BELT | 8 | 343 | 2,741 | LIMESTONE | 200 | 159 | 435,708 | 0.0029 | 0.0014 | C | 48% | 50% | 0% | 90% | 0.02 | 0.03 | 0.01 | 0.02 |
| F 7 | #1 INCLINE BELT | #2 INCLINE BELT | 8 | 343 | 2,741 | LIMESTONE | 200 | 199 | 544,635 | 0.0029 | 0.0014 | C | 48% | 50% | 0% | 60% | 0.12 | 0.16 | 0.06 | 9,08 |
| F 14 | #2 INCLINE BELT | SCREEN #1 | 8 | 361 | 2,891 | LIMESTONE | 200 | 188 | 544,635 | 0.0029 | 0.0014 | ¢ | 48% | 20% | 0% | 90% | 0.04 | 0.06 | 0.02 | 0.03 |
| F 15 | SCREEN #1 | CROSS CTRY, BELT | 8 | 361 | 2.891 | LIMESTONE | 200 | 151 | 435,708 | 0.0029 | 0.0014 | T c | 48% | 20% | 0% | 90% | 0.04 | 0.05 | 0.02 | 0.02 |
| F 16 | SCREEN #1 | HAMMER MILL | 8 | 361 | 2.891 | LIMESTONE | 200 | 38 | 108,927 | 0.0007 | 0.0003 | C | 48% | 20% | 0% | 90% | 0.00 | 0.00 | 0.00 | 0.00 |
| F 17 | HAMMER MILL | #1 INCLINE BELT | B | | | LIMESTONE | 200 | 38 | 108,927 | 0.0029 | 0.0014 | | 48% | 50% | 0% | 90% | 0.01 | 0.01 | 0.00 | 0.00 |
| FIB | CROSS CTRY, BELT | BELT 8 | 8 | 361 | | LIMESTONE | 200 | 151 | 435,708 | 0.0029 | 0.0014 | | 48% | 20% | 0% | 0% | | 0.51 | 0.17 | 0.24 |
| F 19 | BELT B | BELT C | <u> </u> | 361 | | LIMESTONE | 200 | 151 | 435,708 | 0.0029 | 0.0014 | | 48% | 20% | 0% | 0% | | 0.51 | 0.17 | 0.24 |
| | BELT C | SILOS (3) | 8 | 361 | | LIMESTONE | 200 | 151 | 435,708 | 0.0029 | 0.0014 | c | 48% | 20% | 0% | 90% | | 0.05 | 0.02 | |
| | LE CRUSHED ROCK: | 10,500 (0) | - 4 | 301 | <u> </u> | 2150201015 | + | 131 | 755,700 | V-0452 | V-W-17 | - | T-70/70 | | - 70 | هيدا | | | T | 7.02 |
| | | CHUTE | | 25 | ~~~ | LIMESTONE | 200 | 200 | 40,000 | 0.0029 | 0.0014 | - c | 48% | 200 | 0% | 0% | 0.47 | 0.05 | 0.22 | 0.02 |
| F 24 | CROSS CTRY, BELT | | 8 | | | | | | | | 0.0014 | | | 20% | <u>\</u> | - V79 | 0.47 | 0.05 | 0.22 | 0.02 |
| F 25 | CHUTE | GROUND | 8 | 25 | 200 | LIMESTONE | 200 | 200 | 40,000 | 0.0029 | 0.0014 | <u> </u> | 48% | 20% | 096 | O% Totals | | 1.49 | 0.92 | 0.72 |
| | | | | | | | - | | | ļ | | <u> </u> | | ļ | | 101013. | 1.34 | 2,70 | V-24 | - V112 |
| IRON : | ORE RECEIVING | , CRUSHING AND | STO | RAGE | : (2000 | Actual) | | | | | | | 1 | 1 | İ | l | 1 | İ | ļ | ļ |
| F 4 | ILOADER | FEEDER | 2 | 18 | 36 | IRON ORE | 200 | 170 | 6,123 | 0.0002 | 0,0001 | ¢ | 48% | 0% | 0% | 80% | 0.01 | 0.00 | 0.00 | 0.00 |
| F 5 | FEEDER | JAW CRUSHER | 2 | 18 | 36 | IRON ORE | 200 | 170 | 6,123 | 0.0007 | 0.0003 | C | 48% | 50% | 0% | 90% | 0.01 | 0.00 | 0.00 | 0.00 |
| F 6 | JAW CRUSHER | #1 INCLINE BELT | 2 | 18 | 36 | IRON ORE | 200 | 170 | 6,123 | 0.0029 | 0.0014 | C | 48% | 50% | 0% | 90% | 0.02 | 0.00 | 0.01 | 0.00 |
| F 7 | #1 INCLINE BELT | #2 INCLINE BELT | 2 | 18 | 36 | IRON ORE | 200 | 170 | 6,123 | 0.0029 | 0.0014 | C | 48% | 50% | 0% | 60% | 0.10 | 0.00 | 0.05 | 0.00 |
| F 8 | #2 INCLINE BELT | #3 INCLINE BELT | 2 | 18 | | IRON ORE | 200 | 170 | 6,123 | 0.0029 | 0.0014 | | 48% | 20% | 0% | | | 0.00 | 0.02 | 0.00 |
| F 9 | W3 INCLINE BELT | SCREEN #2 | 2 | 18 | | IRON ORE | 200 | 170 | 6,123 | 0.0313 | 0.0150 | | 48% | | 0% | | | 0.01 | 0.20 | |
| F 10 | SCREEN #2 | CROSS CTRY, BELT | 2 | 18 | | IRON ORE | 200 | 170 | 6,123 | 0.0029 | 0,0014 | | 48% | 20% 20% | 0% | | | 0.00 | | |
| FIII | SCREEN #2 | CONE CRUSHER | 1 2 | | | IRON ORE | | n/a | | 0.0029 | 0.0014 | | 48% | 20% | 0% | | | | 1 . | |
| F 112 | CONE CRUSHER | #4 INCLINE BELT | 2 | 1 0 | | IRON ORE | 1 . | n/a | ł | 0.0029 | 0.0014 | | 48% | 20% | 0% | 09 | , | ! | ·• | - |
| F 13 | #4 INCLINE BELT | #2 INCLINE BELT | 1 ž | | · | IRON ORE | 1 | n/a | | 0.0029 | 0.0014 | | 489 | 20% | 0% | 090 | | | | |
| F 14 | #2 INCLINE BELT | SCREEN #1 | 1 2 | | | RON ORE | 200 | 170 | 6,123 | 0.0313 | 0.0150 | | 48% | | 0% | 909 | | 0.01 | 0.20 | |
| F 15 | SCREEN #1 | CROSS CTRY, BELT | 1 2 | | | IRON ORE | 200 | 170 | 6,123 | 0.0029 | 0.0014 | | 48% | 20% | 0% | 90% | | 0.00 | | |
| F 16 | SCREEN #1 | HAMMER MILL | 1 2 | | | IRON ORE | 200 | 170 | 6,123 | 0.0007 | 0.0003 | | 489 | | | | | 0.00 | | |
| F 17 | HAMMER MILL | #1 INCLINE BELT | 1 2 | | | IRON ORE | 200 | 170 | 6,123 | 0.0029 | 0.0014 | | | | | | | 0.00 | | |
| | | | 2 | | | IRON ORE | 200 | 170 | 6,123 | 0.0029 | | | 48% | | Q7 | | | | | |
| F 18 | CROSS CTRY, BELT | IBELT B | | | | | | 170 | | | | | | | 0% | | | | | |
| F 19 | BELT B | BELT C | 2 | | | IRON ORE | 200 | | 6,123 | 0.0029 | | | 48% | | 09 | 07 | | | | |
| F 20 | BELT C | SILOS (3) | 1 2 | 18 | 36 | IRON ORE | 200 | 170 | 6,123 | 0.0029 | 0.0014 | <u> </u> | 489 | 20% | 09 | | | 0.00 | | |
| | | | + | . ' | <u> </u> | <u> </u> | - | | | | | - | <u> </u> | <u> </u> | <u> </u> | Totals | : 1.97 | <u> </u> | 0.95 | 1 0.04 |
| | ECEIVING, CRUSHING | | | 4 | | <u> </u> | | | | 1 | | <u> </u> | | <u> </u> | 1 | - | | | | + |
| F 4 | LOADER | FEEDER | 4 | | | SILICA | 200 | 200 | 43,571 | 0.0002 | 0,0001 | | 489 | | | | | 0.00 | | |
| F 5 | FEEDER | JAW CRUSHER | 4 | | | SILICA | 200 | 200 | 43,571 | 0.0007 | 0.0003 | | 489 | | | | | 0.00 | | |
| F 6 | JAW CRUSHER | #1 INCLINE BELT | 4 | | | SILICA | 200 | 200 | 43,571 | 0.0029 | 0.0014 | | 489 | | 09 | 909 | | | | |
| F 7 | #1 INCLINE BELT | #2 INCLINE BELT | 4 | | | SILICA | 200 | 200 | 43,571 | 0.0029 | 0.0014 | | 489 | | | 609 | | | | |
| FB | #2 INCLINE BELT | #3 INCLINE BELT | 4 | 55 | | SILICA | 200 | 200 | 43,571 | 0.0029 | 0.0014 | | 489 | | 09 | 909 | | | | |
| F 9 | #3 INCLINE BELT | SCREEN #2 | 4 | | 218 | SILICA | 200 | 200 | 43,571 | 0.0313 | | | 489 | | | 909 | | | | 1 0.03 |
| FIO | SCREEN #2 | CROSS CTRY, BELT | 4 | | 218 | SILICA | 200 | 200 | 43,571 | 0.0029 | | | 489 | | . 09 | 909 | | | | |
| F 11 | SCREEN #2 | CONE CRUSHER | 4 | | | SILICA | 200 | 200 | 43,571 | 0,0007 | 0.0003 | C | 489 | 209 | | 909 | | | | |
| F 12 | CONE CRUSHER | #4 INCLINE BELT | 1 4 | | | SILICA | 200 | 200 | 43,571 | 0.0029 | 0.0014 | C | 489 | | . 09 | 6 09 | | | | |
| | M4 INCLINE BELT | #2 INCLINE BELT | | | | SILICA | 200 | 200 | | | | | 489 | | | 6 09 | 6 0.47 | 0.05 | 0.2 | |
| F 13 | | BELT B | 1-7 | - | | SILICA | 200 | 200 | | | | | ··· | | | | 6 0.47 | 0.05 | 0.2 | 2 0.02 |
| F 18 | CROSS CTRY. BELT | BELT C | 1 7 | | | SILICA | 200 | 200 | | 0.0029 | | | ··• | | | | 6 0.47 | | 0.2 | 2 0.02 |
| F 19 | BELT B | | ··• | | | SILICA | 200 | 105 | | | | | 489 | | | 909 | 6 0.02 | | | |
| F 20 | BELTC | SILOS (3) | 4 | | | | 200 | | | | | | 489 | | 09 | 6 09 | | | | |
| F 24 | CROSS CTRY. BELT | CHUTE | <u> </u> | 13 | <u>. 100</u> | SILICA | | +20 | 1 72.3/1 | J.,0023 | . A. | | 4 :73-7 | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |

| | | mran, mayar ru | 1 | | | THROUGHP | | | | | FI | HISSIA | N FACTO |)RS | | | , | EMIS | SIONS | |
|----------------|---------------------|--------------------------------|--------------|---|----------|-------------|-------------|-------------|------------------|--|-----------|-------------|-------------|----------|--------------|-----------------|---------------------------------------|---|----------|----------|
| SOURCE | DESCRIPTION | | HRS | DAYS | HRS | FFENOVGESF | MAX | AVG. | | TSP | PM10 | | PM10 | | CONTRO | L | TSP PM10 | | | 10 |
| | NAME FROM | NAME TO | | /YR | | MATERIAL | TON/H | | TON/YR | LB/TON | LB/TON | REF | | | | | | T/YR | LB/HR | T/YR |
| | S, BLASTING AND DOZ | | † <u>***</u> | 1 | £ 111 | | 7.77 | | | , p. 2. 1 W11 | W 1 PM | · · · · · · | 4.5.77 **** | | | | | <u> </u> | <u> </u> | |
| FII | DRILLING | | 24 | 0 | 320 | LIMESTONE | | | 435,708 | 0.0003 | 0.0001 | | 36% | 0% | 0% | 0% | · · · · · · · · · · · · · · · · · · · | 0.06 | 1 | 0.02 |
| F 2 | BLASTING | | 24 | | | LIMESTONE | | | 435,708 | | Ţ | Б | | 0% | 0% | 096 | l | | | |
| F 3 | DOZING | D9L | 1 | | | LIMESTONE | | | 435,708 | 0.0029 | 0.0014 | C | 48% | | | | | 0.00 | | 0.00 |
| | | DION | 1 | 1 | | LIMESTONE | | | 435,708 | 0.0029 | 0.0014 | 1 | 48% | | **** | | | 0.00 | | 0.00 |
| <u> </u> | | | · | 1 | | | | | | | | 1 | | <u> </u> | | Totals: | · | 0.06 | | 0.02 |
| LIMESTO | NE RECEIVING, CRUSI | HING AND STORAGE | | 1 | | | · | · · · · · · | | | | 1 | | | | | ļ | *************************************** | 1 | |
| F 4 | LOADER | FEEDER | 8 | 343 | 2.741 | LIMESTONE | 200 | 159 | 435,708 | 0.0002 | 0.0001 | C | 48% | 0% | 0% | 80% | 0.01 | 0.01 | 0.00 | 0.00 |
| F 5 | FEEDER | JAW CRUSHER | 8 | | | LIMESTONE | 200 | 159 | 435,708 | 0.0007 | 0.0003 | | 48% | 50% | 0% | 90% | 0.01 | 0.01 | 0.00 | 0.00 |
| F 6 | JAW CRUSHER | #1 INCLINE BELT | 8 | 343 | 2.741 | LIMESTONE | 200 | 159 | 435,708 | 0.0029 | 0.0014 | c | 48% | 50% | 0% | 90% | 0.02 | 0,03 | 0.01 | 0.02 |
| F 17 | #1 INCLINE BELT | #2 INCLINE BELT | 8 | 343 | | LIMESTONE | 200 | 199 | 544,635 | 0.0029 | 0.0014 | T c | 48% | 50% | 0% | 60% | 0.12 | 0.16 | 0.06 | 9.08 |
| F 14 | #2 INCLINE BELT | SCREEN #1 | 8 | 361 | 2.891 | LIMESTONE | 200 | 188 | 544.635 | 0.0029 | 0.0014 | C | 48% | 20% | 0% | 90% | 0.04 | 0.06 | 0.02 | 0.03 |
| F 15 | SCREEN #1 | CROSS CTRY, BELT | 8 | | | LIMESTONE | 200 | 151 | 435,708 | 0.0029 | 0.0014 | | 48% | 20% | 0% | 90% | 0.04 | 0.05 | 0.02 | 0.02 |
| F 16 | SCREEN #1 | HAMMER MILL | 8 | | | LIMESTONE | 200 | 38 | 108,927 | 0.0007 | 0.0003 | C | 48% | 20% | 0% | 90% | 0.00 | 0.00 | 0.00 | 0.00 |
| F 17 | HAMMER MILL | #1 INCLINE BELT | 8 | | | LIMESTONE | 200 | 38 | 108.927 | 0.0029 | 0.0014 | | 48% | 50% | 0% | 90% | | 0.01 | 0.00 | 0.00 |
| F 18 | CROSS CTRY. BELT | BELT B | 8 | 361 | 2,891 | LIMESTONE | 200 | 151 | 435,708 | 0.0029 | 0.0014 | ¢ | 48% | 20% | 0% | 0% | 0,35 | 0.51 | 0.17 | 0.24 |
| F 19 | BELT 8 | BELTC | 8 | | | LIMESTONE | 200 | 151 | 435,708 | 0.0029 | 0.0014 | | 48% | | 0% | | | 0.51 | 0.17 | 0.24 |
| F 20 | BELT C | SILOS (3) | 8 | 361 | 2,891 | LIMESTONE | 200 | 151 | 435,708 | 0,0029 | 0.0014 | C | 48% | | 0% | | | 0.05 | 0.02 | 0.02 |
| | LE CRUSHED ROCK: | | | I | | | | | | | | | | | | 1 | | | | |
| F 24 | CROSS CTRY, BELT | CHUTE | 8 | | 200 | LIMESTONE | 200 | 200 | 40,000 | 0.0029 | 0.0014 | E | 48% | 20% | 0% | 0% | 0.47 | 0.05 | 0.22 | 0.02 |
| F 25 | CHUTE | GROUND | 8 | 25 | 200 | LIMESTONE | 200 | 200 | 40,000 | 0.0029 | 0.0014 | C | 48% | | 0% | 0% | 0.47 | 0.05 | 0.22 | 0.02 |
| | | | | | | L | | | | | | | | | | Totals | 1,91 | 1.49 | 0.92 | 0.72 |
| IRON | ORE RECEIVING | , CRUSHING AND |) STO | RAGE | : (Pote | ntial) |] | | | | | 1 | | 1 | | | l | | | |
| F 4 | LOADER | FEEDER | 2 | 18 | 36 | IRON ORE | 200 | 194 | 7.000 | 0,0002 | 0.0001 | T E | 48% | 0% | 0% | 60% | 0.01 | 0.00 | 0.00 | 0,00 |
| F 5 | FEEDER | JAW CRUSHER | 7 2 | *************************************** | | IRON ORE | 200 | 194 | 7,000 | 0.0007 | 0.0003 | | 48% | | 0% | | | 0.00 | | 0.00 |
| F 6 | JAW CRUSHER | #1 INCLINE BELT | 2 | | | IRON ORE | 200 | 194 | 7,000 | 0.0029 | 0.0014 | | 48% | | | | | | | 0.00 |
| F 7 | #1 INCLINE BELT | #2 INCLINE BELT | 2 | | | IRON ORE | 200 | 194 | 7,000 | 0.0029 | 0.0014 | | 48% | 50% | 0% | | | 0.00 | | 0.00 |
| F 8 | #2 INCLINE BELT | #3 INCLINE BELT | 2 | 18 | 36 | IRON ORE | . 200 | 194 | 7,000 | 0.0029 | 0.0014 | | 48% | 20% | 0% | | | | | 0.00 |
| F 9 | #3 INCLINE BELT | SCREEN #2 | 2 | | | IRON ORE | 200 | 194 | 7,000 | 0.0313 | 0.0150 | C | 48% | 20% | 09 | 909 | 0.49 | 0.01 | | |
| F 10 | SCREEN #2 | CROSS CTRY, BELT | 2 | | | IRON ORE | 200 | 194 | 7,000 | 0.0029 | 0.0014 | | 48% | | 0% | 90% | 0.05 | 0.00 | 0.02 | 0.00 |
| F 11 | SCREEN #2 | CONE CRUSHER | 2 | | | IRON ORE | - | n/a | | 0.0029 | 0.0014 | | 48% | | 090 | | | | | |
| F 12 | CONE CRUSHER | #4 INCLINE BELT | 2 | | | IRON ORE | <u> </u> | n/a | <u> </u> | 0.0029 | 0.0014 | | 48% | | 0% | 0% | | | | |
| F 13 | #4 INCLINE BELT | #2 INCLINE BELT | 2 | | | IRON ORE | <u> </u> | n/a | | 0.0029 | 0.0014 | | 48% | | | 09 | | | | <u> </u> |
| F 14 | #2 INCLINE BELT | SCREEN #1 | 2 | | | IRON ORE | 200 | 194 | 7,000 | 0.0313 | 0.0150 | | 489 | | | | | | | |
| F 15 | SCREEN #1 | CROSS CTRY, BELT | 2 | | | IRON ORE | 200 | 194 | 7,000 | 0.0029 | 0.0014 | | 469 | | | | | | | 0.00 |
| F 16 | SCREEN #1 | HAMMER MILL | 1 2 | | | IRON ORE | 200 | 194 | 7,000 | 0.0007 | 0,0003 | | 489 | | | | | | | 0,00 |
| F 17 | HAMMER MILL | #1 INCLINE BELT | 2 | | | IRON ORE | 200 | 194 | 7,000 | 0.0029 | 0,0014 | | 489 | | | | | | | |
| F 18 | CROSS CTRY, BELT | BELT B | 2 | | | IRON ORE | 200 | 194 | 7,000 | 0.0029 | 0.0014 | | 489 | | | | | | | |
| F 19 | BELT B | BELT C | 2 | | | IRON ORE | 200 | 194 | 7,000 | 0.0029 | 0.0014 | | 489 | | | | | | | |
| F 20 | BELT C | SiLOS (3) | 2 | 18 | 36 | IRON ORE | 200 | 194 | 7,000 | 0.0029 | 0.0014 | ¢ | 489 | 209 | 09 | 6 909 Totals | | | | |
| eii 124 - | TOTIVING AGUEUMA | AND STORES | | | <u> </u> | | | | | | <u> </u> | | 4 | | - | 10(815 | | 1 0.04 | 1.00 | V.02 |
| | ECEIVING, CRUSHING | | 4 | 1 | 1 210 | SILICA | 200 | 200 | 43,571 | 0.0002 | 0.0001 | + | 400 | , | 00 | / 9/10 | i 0.01 | 0.00 | 0.00 | 0.00 |
| F 4 | LOADER | FEEDER | 1 2 | | | | 200 | 200 | | 0.0002 | 0.0003 | | 489 | | . 09 . 09 | | | | | |
| F 5 | FEEDER JAW CRUSHER | JAW CRUSHER #1 INCLINE BELT | 1 7 | | | SILICA | 200 | 200 | 43,571 43,571 | 0.0029 | | | 489 | | | | | | | |
| F 6 | #1 INCLINE BELT | #2 INCLINE BELT | 1 7 | | | SIUCA | 200 | 200 | 43,571 | 0.0029 | | | 489 | 509 | 09 | | | | | |
| F 8 | #2 INCLINE BELT | #3 INCLINE BELT | 1 4 | | | SILICA | 200 | 200 | 43,571 | 0.0029 | 0.0014 | | 489 | | | | | | | |
| FG | #3 INCLINE BELT | SCREEN #2 | 1 4 | | | SILICA | 200 | 200 | 43,571 | 0.0313 | 0.0150 | | 489 | | | | | | | |
| F 10 | SCREEN #2 | CROSS CTRY, BELT | 1 4 | | | SILICA | 200 | 200 | | 0.0029 | | | 489 | | | | | | | |
| F 11 | SCREEN #2 | CONE CRUSHER | 1 4 | | | SILICA | 200 | 200 | | 0.0007 | | | 489 | | | | | | | |
| F 12 | CONE CRUSHER | #4 INCLINE BELT | 1 4 | | | SILICA | 200 | | | 0.0029 | | | 489 | 6 209 | 6 09 | | | | | |
| F 13 | #4 INCLINE BELT | #2 INCLINE BELT | 1 4 | | | SILICA | 200 | 200 | | 0.0029 | | | 489 | | | 6 09 | | | | |
| F 18 | CROSS CTRY. BELT | BELT B | + 4 | | | SILICA | 200 | | | 0.0029 | | | 489 | | | | 6 0.4 | | | |
| F 19 | BELT B | BELT C | 1 4 | | | SILICA | 200 | 200 | | 0.0029 | | | 489 | | | | | | | |
| F 20 | BELT C | SILOS (3) | 4 | | | SILICA | 200 | | | | | | 489 | | | | | | | |
| F 24 | CROSS CTRY, BELT | CHUTE | 1 8 | | | SILICA | 200 | | | | | | 489 | | | | | | | |
| IT 144 | ICHOOS CIRT, DELI | IGUALE | <u> </u> | | | 14461441 | : | , ,,,,,,0 | · | ************************************** | * ******* | | | т. | × | M | | | | |

| П | | | | | THROUGHPUT | | | | | | | EMISSIONS | | | | | | | | | |
|----|---------|----------------------------|--|----------|------------|------------|--------------|----------|----------|----------|------------|------------|----------|----------------|-----------|--------|---------------|-------|--------|-------|-------|
| 50 | WRCE | DESCRIPTION | | HRS | DAYS | HRS | | MAX, | AVG. | | TSP | PM10 | <u> </u> | PM10 | | CONTRO | L . | TS | jp e | PM | |
| CC | DE | NAME FROM | NAME TO | /DAY | /YR | /YR | MATERIAL | TON/H | TON/H | TON/YR | LB/TON | LB/TON | REF | FRAC. | MOIST. | CAPT. | BUILD. | LB/HR | T/YR | LB/HR | T/YR |
| F | | | PACKER #3 | 24 | 0 | | Masonry | 150 | n/a | | 0.2700 | 0.1350 | | 50% | 0% | 95% | 99% | | + | | 7 |
| | | | SPILL SCREW | 24 | 0 | - | Masonry | 150 | n/a | | 0.2700 | 0.1350 | ŧ | 50% | 0% | 95% | | | ٠ | | |
| E | | | ELEVATOR #3 | 24 | 0 | | Masonry | 150 | | | 0.2700 | 0.1350 | e | 50% | 0% | 95% | | - | 4. | - | |
| F | 238 | ELEVATOR #3 | BIN #3 | 24 | 0 | • | Masonry | 150 | n/a | - | 0.2700 | 0.1350 | e | 50% | 0% | 95% | 99% | | - | · | - |
| | | | | | | | | | | | İ | | L | | | | Totals: | 13.55 | 3,50 | 6.78 | 1,75 |
| | | | | | | | | | | | | | I | | | | |] | | | |
| | | <u>n factor references</u> | | | | | | | | | | | | | | | <u>UMMARY</u> | | | | |
| | | 05-020-10 for PM10, er | | | | | | | | | | | | | | | DOZING | | 0.06 | 1 | 0.02 |
| | | 1/95, last paragraph of | Section 11.19.2: Emiss | ion fac | tor esti | mates for | stone quarry | | <u> </u> | | <u> </u> | LIMESTON | | | | | | | 1.49 | 0.92 | 0.72 |
| | blastin | | <u> </u> | L | | · | <u> </u> | | | <u> </u> | IRON ORE | RECEIVING, | | | | | | | 0.04 | 0.95 | 0.02 |
| | | 1/95, Table 11.19.2-2 | | | <u></u> | | <u> </u> | | | <u></u> | <u> </u> | | | | | | STORAGE | | 0,39 | 2.25 | 0.19 |
| | | nmental Quality Manage | ment, Inc., 1995; based | upon h | I-vol sa | mpling stu | xty et | | <u> </u> | <u> </u> | <u> </u> | | | | | | STORAGE | | 0.12 | 1.03 | 0.06 |
| | | Cement, FL in 1989. | | <u> </u> | | | | | | <u></u> | <u> </u> | ILO WITHDE | MAL | CONVE | | | | | 0.21 | 0.02 | 0.10 |
| 0 | AP-42 | 1/95, Table 11.12-2 for | r PM, engineering judger | ment to | r PM10 | | | <u> </u> | | | | <u> </u> | <u> </u> | <u> </u> | | | ANDLING | | 0.35 | 1.21 | 0.17 |
| | | | <u> </u> | ļ | | | <u> </u> | | <u> </u> | | #1 & #2 CL | INKER COOL | ERS A | <u>ND CLIN</u> | | | | | 78.65 | 14.89 | 37.65 |
| | | | | ļ | <u> </u> | | <u> </u> | | <u> </u> | <u> </u> | | | <u> </u> | | | | RECLAIM | | 45,96 | 5.40 | 22.98 |
| Ш | · | | | ļ | | | | | <u> </u> | | <u> </u> | <u> </u> | 1 | | | | ANDLING | | 1.55 | 0.91 | 0.77 |
| | | | | | | | <u> </u> | | | | | FINISH | GRINE | ING AN | | | ANDLING | | 3.79 | 1.43 | 1.77 |
| | | <u></u> | | | | | <u> </u> | | <u> </u> | | 4 | <u> </u> | | | <u>Cl</u> | | DADOUT | | 3.50 | 6.78 | 1.75 |
| ш | | <u> </u> | <u>i </u> | L | 1 | | 1 | | <u> </u> | l | <u> </u> | | | <u> </u> | <u> </u> | GRAN | ID TOTAL | 90.52 | 136,12 | 35,79 | 66.20 |

APPENDIX B

Carbon Monoxide Modeling Review

MEMORANDUM

TO: Zach Klotovich, Associate Air Quality Engineer, State Office of Technical Services

FROM: Kevin Schilling, Air Quality Scientist, State Office of Technical Services

SUBJECT: Carbon Monoxide Modeling Review for Kilns at the Ash Grove Cement Company Facility;

Inkom, Idaho

DATE: July 19, 2002

1. SUMMARY:

Ash Grove Cement Company requested a modification of the kiln carbon monoxide (CO) emissions limits in the Tier II operating permit for their Inkom, Idaho facility. Ash Grove was requested to demonstrate that CO emissions from the facility would not cause or significantly contribute to a violation of an ambient air quality standard, as required by IDAPA 58.01.01.403.02.

The Idaho Department of Environmental Quality (DEQ) has reviewed the analyses and supporting materials submitted, and has verified that operation of the kilns as specified in the consent order will satisfy the requirements of IDAPA 58.01.01.403.02.

2. DISCUSSION:

2.1 Introduction and Regulatory Requirements for Modeling

On June 10, 2002 a consent order became effective that amended Ash Grove's Tier II operating permit (issued on December 8, 1997) and a Permit to Construct (PTC)(issued on January 29,1999). The consent order clarified that the CO emissions limits of Kiln #1 (234.4 pounds per hour {lb/hr}) and Kiln #2 (275.8 lb/hr) were based on a 1-hour averaging period. Ash Grove also submitted a request to increase the allowable hourly emissions limits to 550 lb/hr CO for Kiln #1 and 650 lb/hr CO for Kiln #2.

Per IDAPA 58.01.01.403, no Tier II operating permit can be granted unless the applicant demonstrates to the satisfaction of DEQ that emissions from the facility "would not cause or significantly contribute to a violation of any ambient air quality standard." Atmospheric dispersion modeling was performed by the applicant's consultant, MFG, to fulfill these requirements.

2.2 Applicable Air Quality Impact Limits and Required Analyses

The Ash Grove facility is located in Bannock County, designated as an attainment or unclassifiable area for CO. If estimated maximum ambient air impacts from the emissions sources at the facility exceed the "significant contribution" levels of IDAPA 58.01.01.006.93, then DEQ modeling guidance requires a full impact analysis. A full impact analysis for attainment area pollutants requires adding ambient impacts from facility-wide emissions to a DEQ-approved background concentration value that is appropriate for each criteria pollutant at the facility location. The resulting CO concentration in ambient air is then compared to the National Ambient Air Quality Standards (NAAQS) listed in Table 1. Table 1 also specifies the modeled value that must be used for comparison to the NAAQS.

2.3 Background Concentrations

Applicable background concentrations are shown in Table 2. Statewide background concentrations used for the Ash Grove CO modeling were provided by DEQ to MFG.

Table 1. Applicable Regulatory Limits

| Pollutant | Averaging Period | Regulatory Limit ^a (μg/m³) ^b | Modeled Value Used ^c |
|----------------------|---------------------|---|--|
| Carbon Monoxide (CO) | 1-hour | 40,000° | Maximum 2 ^{no} highest at any |
| | 8-hour | 10,000 ⁸ | modeled receptor |

IDAPA 58.01.01.577

b. Micrograms per cubic meter

When using five years of meteorological data

Not to be exceeded more than once per year

Table 2. Background Concentrations

| Pollutant | Averaging Period | Background Concentration (µg/m³) ^a |
|----------------------|------------------|--|
| Carbon Monoxide (CO) | 1-hour | 11,500 |
| | 8-hour | 5,200 |

Micrograms per cubic meter

2.4 Modeling Impact Assessment

The ambient air impact analysis was performed by MFG using the model ISC-PRIME - Version 99020. A modeling protocol was not submitted to DEQ prior to the analysis. DEQ conducted verification modeling using ISC-PRIME - Version 99020. Table 3 provides a summary of the modeling parameters used for the DEQ analysis. Figure 1 shows the revised receptor grid used for the modeling analysis. Upper air data were not available for 1995, the year when surface data are available. Therefore, the upper air data were generated from the average monthly morning and evening mixing heights from the Boise, Idaho, seven-year data set. The U.S. Environmental Protection Agency (EPA) meteorological preprocessor program MPRM was then used to generate hour-by-hour mixing heights for model input.

Table 3. Modeling Parameters

| Parameter | Description/Values | Documentation/Additional Description | |
|----------------------------------|--|---|--|
| Model | ISCST3 | Version 99020 | |
| Meteorological Data | Inkom, Idaho (surface); Boise, Idaho (upper air) | 1995 for surface; 1984-1991 upper air | |
| Model Options | Regulatory Default | | |
| Land Use | Rural | Based on population density and actual land use | |
| Terrain | Simple and Complex | Elevation data from digital elevation model (DEM) files: Fx11_75ma.dem and Fx11_75m.dem | |
| Building Downwash | Used Building Profile Input Program (BPIP) | Building dimensions obtained from modeling files submitted | |
| Receptor Grids (See Figure 1) | Grid 1 | 50 meter spacing along property boundary and along roads through the property | |
| | Grid 2 | 10 km by 8 km grid with 250 meter spacing | |
| • • | Grid 3 | 2.5 km by 2.5 km grid with 50 meter spacing near the kilns | |
| Facility Location | Easting | 397.8 kilometers | |
| (UTM) | Northing | 4,738.1 kilometers | |

Tables 4 and 5 provide emissions quantities and other emissions parameters. Stack location, stack height, stack diameter, stack gas temperature, and stack gas flow rate were provided by MFG.

Building and tank dimensions provided in the Building Profile Input Program (BPIP) file were compared against the scaled plot plan and the effect of buildings and tanks on plume downwash was included in the analysis.

Table 4. Emissions Quantities

| Source | Maximum Hourly Emissions Rate ^a pounds per hour (lb/hr) |
|-----------|--|
| Pollutant | CO |
| Kiln #1 | 550 |
| Kiln #2 | 650 |

Emissions rate used for 1-hour and 8-hour averaging periods

Table 5. Emissions and Stack Parameters

| Source | Source Type | Stack Height (m)* | Stack Diameter (m) | Stack Gas Temp. (K) ⁵ | Stack Gas Flow Velocity (m/sec) ^c |
|---------|----------------|-------------------------|--------------------------|---|---|
| Kiln #1 | Point | 22.56 | 1.83 | 519 | 7.06 |
| Kiln #2 | Point | 22.56 | 1.83 | 464 | 7.18 |

- Meters
- b. Kelvin
- c. Meters per second

A significant impact analysis was initially performed to determine if emissions from the facility would "significantly contribute" to pollutant concentrations in ambient air, as per IDAPA 58.01.01.006.93. A full impact analysis was then performed if emissions from the facility that were estimated to have an ambient impact exceeding "significant contribution" levels. The full impact analysis involved modeling impacts from the facility's emissions and adding those impacts to background concentrations.

3. MODELING RESULTS:

Modeled ambient air impact results from the significant impact analysis are provided in Table 6 for CO emissions. Because the potential ambient impact of the facility-wide emissions exceeds "significant contribution" levels for 1-hour and 8-hour CO, a full impact analysis was performed for those averaging times.

Table 6. Significant Impact Analysis for Criteria Pollutants (Facility-wide Emissions)

| Pollutant | Averaging Period | Amblent concentration (μg/m³) | Significant Contribution ^a (µg/m³) | Full Impact Analysis Required (Y or N) |
|-----------|---------------------|-------------------------------------|---|--|
| CO | 1-hour | 8,600 ^b | 2,000 | . Y |
| · | 8-hour | 3,500° | 500 | Y |

Significant contribution level as per IDAPA 58.01.01.006.93

Results of the full impact analysis are presented in Table 7 and indicate that operation of the facility as described in the consent order will not cause or significantly contribute to a violation of an applicable NAAQS. Figures 2 and 3 show the maximum-modeled CO 1-hour and 8-hour averaged concentration impacts, respectively.

Electronic copies of the modeling analysis are saved on disk. Table 8 provides a summary of the files used in the modeling analysis. The permitting engineer has reviewed this modeling memo to ensure consistency with the Tier II operating permit and technical memorandum.

Maximum 2nd highest modeled value at any receptor

Table 7. Full Impact Analysis for Criteria Pollutants (Facility-wide Emissions)

| Pollutant | Averaging Period | Ambient Conc. (μg/m³)* | Background Conc. (μg/m³) | Total Ambient Conc. (μg/m³) | Regulatory Limit ^b (μg/m³) | Compliant (Y or N) |
|------------------|---------------------|------------------------------|--------------------------------|--------------------------------------|---|-----------------------|
| Carbon | 1-hour | 8,600 ^c | 11,500 | 20,100 | 40,000 | Y |
| Monoxide (CO) | 8-hour | 3,500 ^e | 5,200 | 8,700 | 10,000 | Y |

Concentration in micrograms per cubic meter IDAPA 58.01.01.577
Maximum 2nd highest modeled value at any receptor

Table 8. Dispersion Modeling Files

| Table 8. Dispersion Modeling Files | | | | | |
|---|--|---------------------|--|--|--|
| Type of File | Description | File Name | | | |
| Met | 1995 Inkom, Idaho for surface data | Inkom95.met | | | |
| Data | average of 1984-1991 Boise, Idaho upper air | | | | |
| BEEST | CO 1-hour and 8-hour | AshGroveCO.BST | | | |
| Input | | | | | |
| Files | | | | | |
| Each BST | file has the following type of files associated with it: | | | | |
| Input fil | e for BPIP program | .PIP | | | |
| BPIP or | utput file | TAB | | | |
| Concise BPIP output file | | .SUM | | | |
| BEE-Line file containing direction specific building dimensions | | s .SO | | | |
| ISCST3 input file for each pollutant | | .DTA | | | |
| ISCST | output list file for each pollutant | LST | | | |
| User su | mmary output file for each pollutant | .USF | | | |
| Master | graphics output file for each pollutant | .GRF | | | |
| Some mod | deling files have the following type of graphics files as: | sociated with them: | | | |
| Surfer o | | .DAT | | | |
| Surfer b | oundary file | .BLN | | | |
| Surfer p | ost file containing source locations | · .TXT | | | |
| Surfer p | olot file | .SRF | | | |

KS: G:\Technical Services\Modeling\Schilling\AshGove\Ash Grove modeling Tech memo.doc

Figure 1 - Ash Grove CO Modeling for Consent Order

Receptor Grid for CO Modeling

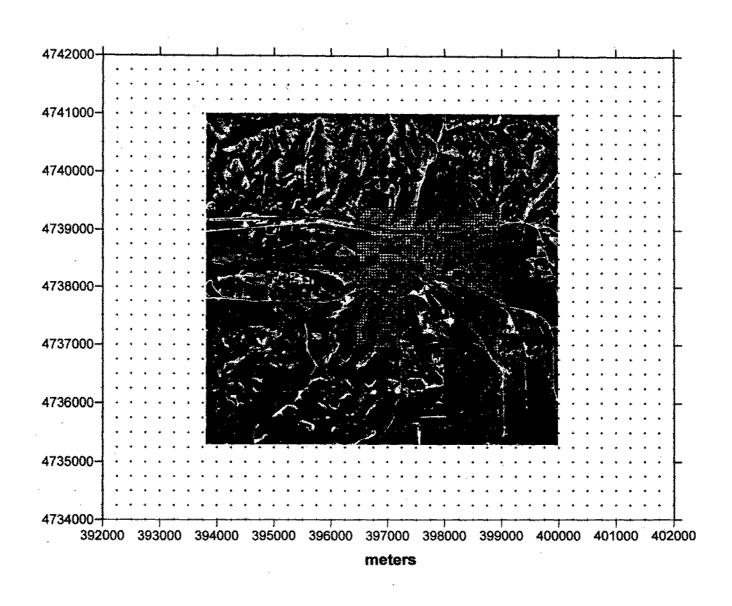


Figure 2 - Ash Grove CO Modeling for Consent Order

2nd Highest 1-Hour Modeled CO Concentrations

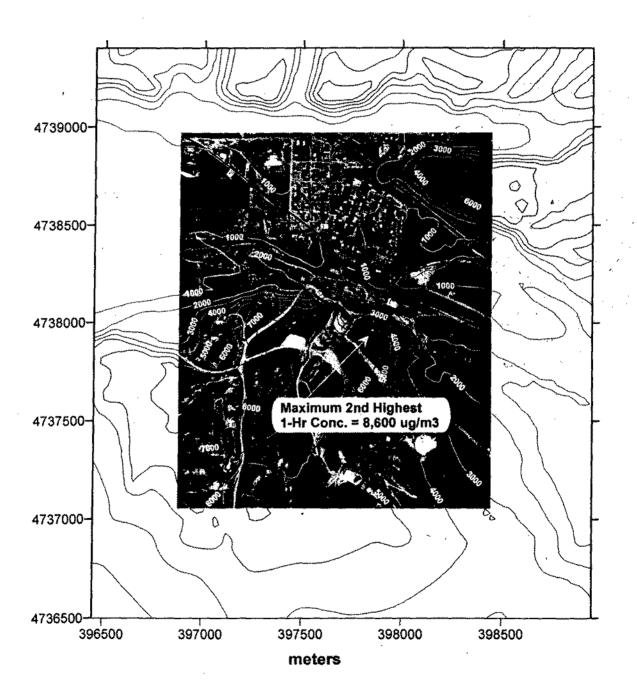
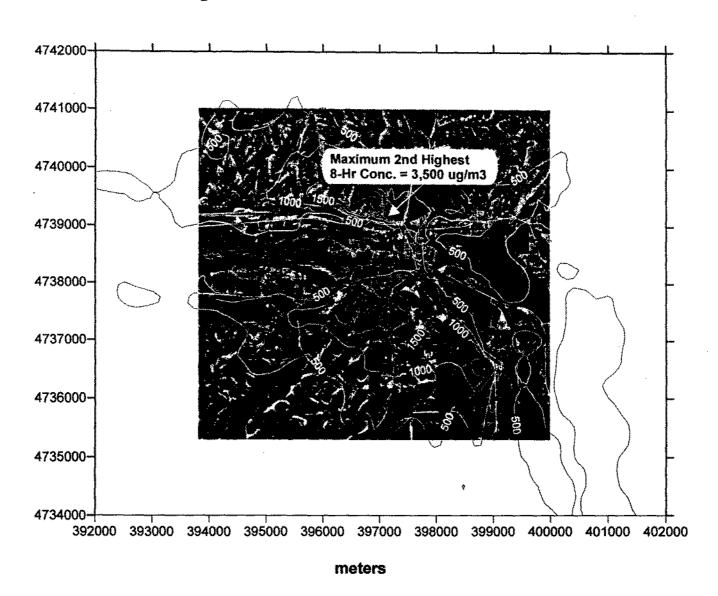


Figure 3 - Ash Grove CO Modeling for Consent Order
2nd Highest 8-Hour Modeled CO Concentrations



APPENDIX C

Public Comments

The following comments on the draft Tier II operating permit were received from Ash Grove Cement Company on September 23, 2002.

The Department's response to each comment is provided in bold.

Comments for Tier II

1) Revise Tier II permit according to Consent Order paragraph 21 which upon execution of the Consent Order immediately modified the existing December 1997 Tier II permit. These changes are not reflected in the draft Tier II modification. Failure to incorporate the modifications set forth in the Consent Order will causes conflict between the Consent Order language and the reissued December 1997 Tier II permit. Specifically, the following revisions to the Tier II were effective upon signing the Consent Order and must be reflected in the proposed modified Tier II for consistency:

Upon the effective date of this Consent Order, the Tier II operating permit issued on December 8, 1997 and the PTC issued on January 29, 1999 shall be amended as follows:

A. Tier II operating permit condition 4.1.2 on page 16 of 35 (Source: #1 and #2 Rotary Kilns) shall be deleted.

Permit condition 4.1.2 was deleted. The deleted condition stated, "Fuel usage, based on fuel heat content, shall be limited to 96 million Btu per hour (MMBtu/hr) and 797,000 MMBtu per yr (MMBtu/yr) for the No. 1 kiln, and to 113 MMBtu/hr and 938,000 MMBtu/yr for the No.2 kiln per applicants submittal." Permit condition 4.1.2 was replaced by the tire feed rate limit discussed in paragraph F below.

B. PTC condition 2.5 on page 3 of 8 (Source: #1 and #2 Clinker Coolers and Process Rates) shall be deleted.

The PTC condition was contained in the draft Tier II operating permit at condition 4.5 on page 28 of 50. The condition was deleted. The deleted condition stated, "The clinker coolers shall process no more than the ton-per-hour production, on a monthly average basis, of the kilns. The clinker coolers shall process no more than the annual production of the kilns."

C. The portions of the December 8, 1997, Tier II operating permit setting forth the short term emissions limitations for particulate matter, nitrogen oxides, and carbon monoxide emitted from Kiln #1 and Kiln #2 shall be amended to impose the following emissions limitations:

Kiln #1

Particulate Matter: 0.3 lb/ton of dry kiln feed Nitrogen Oxides: 144 lb/hr based upon a 12 month rolling average Carbon Monoxide: 234.4 lb/hr based upon a 1 hour average

Kiln #2

Particulate Matter: 0.3 lb/ton of dry kiln feed Nitrogen Oxides: 193 lb/hr based upon a 12 month rolling average Carbon Monoxide: 275.8 lb/hr based upon a 1 hour average

The emission limits were amended. The carbon monoxide limits were set at 550 lb/hr for kiln #1 and 650 lb/hr for kiln #2 as requested by Ash Grove and as allowed by consent order condition 21.E. The modeling analysis for the increased carbon monoxide emission limits is provided in Appendix B of the technical memorandum.

D. Compliance with the emission limits set forth in paragraph 21.C of this Consent Order shall be ascertained by compliance with paragraphs 7-11 of this Consent Order. Paragraphs 7, 8, 9, and 11 of the consent order were incorporated into the Tier II operating permit. Paragraph 10 of the consent order was not incorporated because it was a one-time testing requirement that has been satisfied.

E. Ash Grove requested a modification of the emission limits and averaging times set forth above for Carbon Monoxide (CO). Upon completion of the Department's review of the submitted data and a determination that modification of the emission limits complies with the National Ambient Air Quality Standard and the Rules for the Control of Air Pollution in Idaho, the Department may modify the emission limitations for CO in paragraph 22.C this Consent Order. The modified emission limitations shall be incorporated into the Tier II and Tier I operating permits.

The modified carbon monoxide emission limits were included in the Tier II operating permit.

F. Ash Grove shall be limited to a tire feed rate of no more than 500 pounds of tire derived fuel per hour based upon a 12 month rolling average on each kiln (specifically, permit condition 4.1 for the #1 and #2 Rotary Kilns is amended to include a new subsection).

The tire feed rate limit was included in the draft permit at condition 4.1.2. on page 25 of 52.

G. The portions of the December 8, 1997 Tier II operating permit setting forth the emissions limitations for the #1 and #2 kilns shall be amended to include the following emissions limitation for organic HAPs (specifically permit condition 2.1 for the #1 and #2 Rotary Kilns is amended to include a new 2.1.4: Appendix A is amended to include a Total HAPs emissions limitation for Kiln #1 and Kiln #2):

Kiln #1 and Kiln #2

Total organic Hazardous Air Pollutant emissions shall not exceed 9.9 tons per year total emissions for both kilns determined on a 12 month rolling average.

Permit Condition 2.1.4 was added to the #1 and #2 Rotary Kilns portion of the Tier II operating permit.

H. The permittee shall demonstrate compliance with the total organic HAPS emission limitation by performing annual Method 25A compliance tests on Kiln #1 and Kiln #2 while burning tires. The annual compliance tests will develop emissions factors for each kiln to be used during the following 12 month period to determine compliance with the annual emission limitation for total organic HAPs from the kilns (specifically permit condition 3 for #1 and #2 Rotary Kilns is amended to include this testing requirement for the kilns). Emissions will be determined for each kiln by the following equation to calculate organic HAP emissions from the kilns:

Total kiln organic HAPs emissions = Organic HAP Emissions (Kiln 1) + Organic HAP Emissions (Kiln 2)

Kiln #1

Tons/yr organic HAP Emissions (Kiln 1) = [lb/hr emissions Kiln No.1 (method 25A) /kiln No. 1 tire feed rate during test (tons/hr)] \times [rolling 12 month No.1 kiln tire feed (tons)/2000]

Kiln #2

Tons/yr organic HAP Emissions (Kiln 2) = [lb/hr emissions Kiln No.2 (method 25A) /kiln No. 2 tire feed rate during test (tons/hr)] x [rolling 12 month No.2 kiln tire feed (tons)/2000]

The requirements of paragraph H were included in the Tier II operating permit at permit condition 3.9 of the #1 and #2 Rotary Kilns portion of the permit.

I. The Tier II operating permit issued pursuant to Paragraphs 19 and 20 shall be subject to public comment and shall require that compliance with the tire feed limits and total organic hazardous air pollutant emission limits set forth in Paragraphs 21.F-H be confirmed using appropriate Method 25A testing.

The Tier II operating permit referenced in Paragraphs 19 and 20 of the consent order has not been drafted yet. Paragraph 21.I will be addressed once the permit is drafted.

In addition, these changes must necessarily be made in the draft Tier I to reflect the currently applicable requirements.

The consent order requirements are contained in the draft Tier I operating permit.

2) Ash Grove suggests that IDEQ take this opportunity of reissuing the Tier II operating permit to renew the permit, which is due to expire in December 2002. Ash Grove suggested that renewal be addressed through the Consent Order process prior to execution of the document in June 2002, but IDEQ did not act at that time. To conserve resources, Ash Grove resubmits the request to renew the existing Tier II, at least for a duration long enough to extend the effectiveness of the modified existing permit until a new Tier II operating permit (required by the Consent Order) is issued.

As noted in IDAPA 58.01.01.404.04, the expiration of a Tier II permit will not affect the operation of a stationary source or a facility during the administrative procedure period associated with the permit renewal process. The administrative procedure period is the time it takes the Department to issue a permit after a complete renewal application has been received. The Tier II permit application required by the consent order will be considered a renewal application and is due on December 8, 2002, the same day the current Tier II will expire. Therefore, the expiration date does not need to be extended.